

POWER SUPPLY MODULE AND ELECTRONIC APPARATUS USING THE SAME

CROSS-REFERENCE TO RELATED APPLICATIONS

This application is based upon and claims the benefit
5 of priority from the prior Japanese Patent Application No.
2003-093880, filed on March 31, 2003, the entire contents
of which are incorporated herein by reference.

BACKGROUND OF THE INVENTION

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1.FIELD OF THE INVENTION

The present invention relates to an on-board type
power supply module for a distributed power supply system
and an electronic apparatus using the same, and more
15 particularly a power supply module for improving power
supply efficiency and an electronic apparatus.

2.Description of the related arts

With increasing complexity of an electronic apparatus
20 such as an information processing unit, the electronic
apparatus is required to have improved reliability. As a
distributed configuration is preferably applied to the
electronic apparatus to obtain improved reliability, a
power supply unit having a distributed configuration is
25 also desired for the electronic apparatus. A distributed
power supply system is currently applied for a server, a
storage system, etc. The distributed power supply system

requires a miniaturized power supply module which can be on-board mounted on a board for electronic units installed in the server, the storage unit, etc.

FIG. 9 is a configuration diagram of a prior art transformer-coupled switching power supply circuit. A primary winding 100 and two secondary windings 110, 120 are wound around a core of a transformer T, enabling transformer coupling between the primary side and the secondary side. The primary side is provided with an FET 102, which is a primary side circuit for controlling the current flowing through the primary winding 100, and a switching control circuit 104.

Meanwhile, on the secondary side, there are provided: pairs of FETs 114, 116 and 124, 126 respectively constituting rectifier circuits which rectify the current flowing through the secondary windings 110, 120; switching control circuits 112, 122; choke coils L1, L3 and capacitors C1, C2 which constitute smoothing circuits.

As is well known, in this switching power supply, switching control circuits 112, 122 controls to switch FETs 114, 116, 124, 126 to perform rectification operation of the secondary output, and to protect from overcurrent and overvoltage. Also, switching control circuit 104 controls FET 102 to protect from overcurrent on the primary side.

In such a way, when a large electric current is required on the secondary side, two secondary circuits are provided, constituting a so-called double-current configuration.

FIG. 10 is an explanatory winding diagram in a conventional power supply module, and FIG. 11 is an exploded configuration diagram of the conventional power supply module. As can be seen from FIGS. 10, 11, there are limits
5 of a card size, component layout, etc. when miniaturizing the power supply module. A typical power supply module is structured of five layers L1 - L5.

A top surface layer L1 and a bottom surface layer L5 are component-mounting layers, while inner layers L2 - L4 are provided for forming circuit patterns. The top surface
10 layer L1 is provided an one part of a transformer T, a primary winding 100 and primary-side circuit 102, 104, FETs 114, 116, 124, 126 of the secondary side circuit, one portion of switching control circuit 112, 122 on the secondary side,
15 one input terminal 150 and one output terminal 160.

The bottom surface layer L5 is provided another part of the transformer T, the primary winding 100 and the primary-side circuit, choke coils L1, L3 and capacitor C disposed in the secondary side circuit, the other portion
20 of the switching control circuit 112, 122 on the secondary side, another input terminal 152 and another output terminal 162.

A first inner layer L2 is provided two secondary windings 110, 120, a wiring area 132 for the primary side
25 circuits 102, 104 and a wiring area 130 for the secondary switching control circuits 112, 122. A second inner layer L3 is provided a pair of output pattern films P1, P3, a

wiring area 136 for the primary side circuits 102, 104 and
a wiring area 138 for switching control circuits 112, 122
on the secondary side. A third inner layer L4 is provided
a pair of ground films G1, G3, a wiring area 138 for the
5 primary side circuits 102, 104 and a wiring area 140 for
switching control circuits 112, 122 on the secondary side.

As shown in FIG. 10, the primary winding 100, the
transformer T, and the pair of the secondary windings 110,
120 are disposed on a module, from left to right on this
10 order. Together with these components, the primary side
circuits 102, 104, the secondary side circuits 114, 116,
124, 126, and L1, L3, the output pattern films P1, P3 and
the ground films G1, G3 are provided.

More specifically, the pair of secondary windings 110,
15 120 is drawn out in the same direction. Also, the secondary
side circuits 114, 116, 124, 126, and L1, L3, the output
pattern films P1, P3 and the ground films G1, G3 are disposed
in such a manner that each point p1, u1, q1, s1, t1, p2,
u2, q2, s2, and t2 in the secondary side circuit shown in
20 FIG. 9 may be connected between the relevant layers through
vias.

Now, in recent years, a load to which power is supplied
from such a power supply module requires a large electric
current. For example, a high-speed CPU requires larger
25 current than a low-speed CPU. When outputting such large
current, the resistance and inductance included in the
patterns of the power supply module become hardly

negligible, because a large power loss and noise may be produced.

According to the above-mentioned layout of the conventional power supply module, the pair of secondary
5 windings 110, 120 is drawn out in single direction, as illustrated in FIG. 10. Therefore, it is difficult to obtain large cross-section areas S of the secondary windings 110, 120. Also, in order to draw in single direction, it is
10 necessary to mount both a pair of rectifier circuits and a pair of smoothing circuits of the secondary side on single side of the transformer T . To enable via connection with these secondary side circuits, the lengths l of the secondary windings 110, 120 have to be large.

The resistance r of the secondary windings is defined
15 as $r = \rho * l / S$, the resistance value of the secondary windings cannot be small enough when l is large. Further, because the drawing of single direction requires a pair of output pattern films and a pair of ground films to be disposed on single side of the transformer T , it is difficult to
20 have wide output pattern films and wide ground films. Therefore, it is difficult to reduce the output resistance.

As a result, when a large current is output, a large power loss is produced, and power supply efficiency is reduced. Further, because of large pattern lengths of the
25 secondary windings, the inductance L becomes large. In the switching power supply, sharp current variation (di/dt) is produced by the choke coil and the transformer, the

produced noise is determined as $L \cdot di/dt$. Accordingly, when the current becomes large, the noise produced becomes hardly negligible, and a large switching noise is produced.

Needless to say, if a size of the power supply module
5 may be large, the resistance value and the inductance of each pattern disposed on the pattern layers L2, L3, L4 can be smaller. However, the power supply module of large size does not fit for an apparatus in which miniaturization is desired.

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SUMMARY OF THE INVENTION

Accordingly, it is an object of the present invention to provide a power supply module and an electronic apparatus
15 of limited size range, and with improved power supply efficiency.

It is another object of the present invention to provide a power supply module and an electronic apparatus which prevent from increasing the power loss, even under a large
20 output current condition.

Further, it is still another object of the present invention to provide a power supply module and an electronic apparatus which prevent from increasing switching noise, even under a large output current condition.

25 In order to attain the aforementioned objects, a power supply module and an electronic apparatus in accordance with the present invention have a power supply module

including a primary winding coupled with secondary windings by a transformer. The power supply module also includes: a component-mounting layer on which the primary winding, the transformer, a primary side circuit, and a secondary
5 side circuit are mounted; a first inner layer on which a pattern of a first secondary winding drawn in one direction is formed; and a second inner layer on which a pattern of a second secondary winding of the secondary windings drawn in the other direction is formed. An output pattern film
10 of the second secondary winding is formed on the first inner layer, and an output pattern film of the first secondary winding is formed on the second inner layer.

According to the present invention, a pair of secondary windings is drawn out in both directions, and provided on
15 different layers. With such a structure, the secondary windings can be formed of wide and short patterns. Also, because of the drawing in both directions, the output pattern films can be disposed on both sides of a second and a third layers, enabling widened output pattern films.

20 With this structure, when an output current becomes large, the power loss becomes half as much as in the conventional power supply module, and thus improved power efficiency can be obtained. Further, because of the reduced inductance, switching noise can be reduced. Moreover, the
25 module can be attained without making the module size large.

According to the present invention, preferably, the power supply module further includes a third inner layer

on which a pair of ground films for the first and the second secondary windings is formed. With this structure, the ground films can be widened, and thus reduced pattern resistance can be obtained.

5 Also, according to the present invention, preferably, on the component-mounting layer, a secondary side circuit of the first secondary winding and a secondary side circuit of the second secondary winding are disposed on both side of the transformer. With this structure, connection to each
10 secondary winding through vias becomes possible, and thus a miniaturized power supply module can be structured.

Further, according to the present invention, preferably, the component-mounting layer includes: a first component-mounting layer on which a rectifier circuit for
15 the secondary side circuit of the first secondary winding is disposed on one side of the transformer and a rectifier circuit for the secondary side circuit of the second secondary winding is disposed on the other side of the transformer; and a second component-mounting layer on which
20 a smoothing circuit for the secondary side circuit of the first secondary winding is disposed on one side of the transformer and a smoothing circuit for the secondary side circuit of the second secondary winding is disposed on the other side of the transformer.

25 With this structure, connection to each secondary winding through via becomes possible, and thus a miniaturized power supply module having short pattern

lengths can be structured.

Also, according to the present invention, preferably, the secondary side circuit mounted on the component-mounting layer, the first secondary winding and the output pattern film formed on the first inner layer, the second secondary winding and the output pattern film formed on the second inner layer, and the pair of ground films formed on the third inner layer are connected through via. With this structure, a miniaturized power supply module having short pattern lengths can be attained.

Still further, according to the present invention, preferably, the rectifier circuit for the secondary side circuit mounted on the component-mounting layer includes a switching element and a switching control circuit. With this structure, switching noise produced in the switching power supply can be reduced.

Further, according to the present invention, preferably, the power supply module includes an input terminal connected to the primary winding, and an output terminal connected to the output pattern film. Thus, the power supply module can be connected to a printed circuit board.

Further scopes and features of the present invention will become more apparent by the following description of the embodiments with the accompanied drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 shows an exploded configuration diagram of a power supply module in accordance with an embodiment of the present invention.

FIG. 2 shows a cross-sectional view of a power supply module in accordance with an embodiment of the present invention

FIG. 3 shows an explanatory diagram of the secondary winding pattern shown in FIG. 1.

FIG. 4 shows cross-sectional views of the transformer, the primary winding, and the secondary winding shown in FIG. 1.

FIG. 5 shows a diagram illustrating a relation between the primary winding and the secondary winding shown in FIG. 1.

FIG. 6 shows a circuit diagram of the power supply circuit shown in FIG. 1.

FIG. 7 shows a configuration diagram of a CPU board, on which the power supply module shown in FIG. 1 is mounted.

FIG. 8 shows a configuration diagram of an electronic apparatus, in which the CPU board shown in FIG. 7 is accommodated.

FIG. 9 shows a circuit diagram of a conventional power supply circuit.

FIG. 10 shows a diagram illustrating a relation between a primary winding and a secondary winding according to a conventional method.

FIG. 11 is an exploded configuration diagram of a

conventional power supply module.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

The preferred embodiment of the present invention is
5 described hereinafter referring to the charts and drawings,
on the order of a power supply module, an electronic
apparatus, and other embodiments.

[Power supply module]

FIG. 1 is a configuration diagram of each layer in
10 a power supply module in accordance with an embodiment of
the present invention. FIG. 2 is a cross-sectional view
of the embodiment of the present invention. FIG. 3 is an
explanatory diagram of a secondary winding pattern shown
in FIG. 1. Also, FIG. 4 is a cross section of a transformer.
15 FIG. 5 is a diagram illustrating a relation between the
primary winding and the secondary winding shown in FIG.
1. And, FIG. 6 is a circuit diagram of the power supply
module shown in FIG. 1.

Before explaining the layout configuration shown in
20 FIG. 1, the circuit configuration of the power supply module
of which layout configuration is shown in FIG. 1 will be
described, referring to FIG. 6. The configuration diagram
shown in FIG. 6 denotes a transformer-coupled switching
power supply circuit, which is similar to that shown in
25 FIG. 9. A primary winding 30 and two secondary windings
40, 50 are wound around a core of a transformer T, and thus
the primary side and the secondary side are transformer

coupled. On the primary side, there are provided, as a primary side circuit, an FET 32 controlling the current flowing through the primary winding 30, and a switching control circuit 34.

5 On the other hand, on the secondary side, there are provided: a pair of FETs 42, 44 and a pair of FETs 52, 54 constituting rectifier circuits each rectifying the current flowing through each secondary winding 40, 50; a switching control circuit 70; choke coils L1, L2 and
10 capacitors C1, C2 constituting smoothing circuits.

As is generally known, in this switching power supply circuit, a switching control circuit 70 supervises the output voltage, and switches FETs 42, 44, 52, 54, so as to perform a rectification operation for the output on the
15 secondary side, and to protect the secondary side from over-current and over-voltage. Also, the switching control circuit 34 controls FET 32 to protect the primary side from overcurrent.

As such, when a large electric current is required
20 on the secondary side, there is adopted so-called a double current configuration, with the provision of two secondary side circuits.

Now, a resistance component and an inductance component respectively produced in the inner layers
25 described earlier are illustrated in FIG. 6. In this figure, r_a and L_a denote the resistance and the inductance of the secondary windings 40, 50; L_c and r_c denote the inductance

and the resistance of an output pattern film; and, L_g and r_g denote the inductance and the resistance of a ground film.

As illustrated in the cross-sectional view of power supply module 10 shown in FIG. 2, this power supply module 10 is provided with five layers $L1 - L5$. A top surface layer $L1$ and a bottom surface layer $L5$ constitute component-mounting layers, while inner layers $L2 - L4$ constitute layers on which patterns are formed.

As shown in FIG. 1, the top surface layer $L1$ is provided: a transformer T ; an portion of a primary winding 30; primary-side circuit portions 32, 34; FETs 42, 44, 52, 54 of the secondary side circuit; the switching control circuit portion 70 on the secondary side; one input terminal 60; and one output terminal 64.

The bottom surface layer $L5$ is provided: the transformer T ; the primary winding 30; the other portion of the primary-side circuit portions 32, 34; choke coils $L1$, $L2$ and a pair of capacitors C which are disposed in the secondary side circuit; the other switching control circuit portions 70 on the secondary side; the other input terminal 62; and the other output terminal 66.

In a first inner layer $L2$, according to the present invention, there is provided a pattern 40 of a first secondary winding, which is drawn out in one direction. And, on its left, a second output pattern film 56 is disposed. Further, there are provided: a wiring area 82 for the primary

side circuits 32, 34; and a wiring area 80 for the secondary-side switching control circuit 70.

In a second inner layer L3, according to the present invention, there is provided a pattern 50 of a second secondary winding, which is drawn out in the other direction than the direction of pattern 40. And, on its right, a first output pattern film 46 is disposed. Further, there are provided: a wiring area 86 for the primary side circuits 32, 34; and a wiring area 84 for the secondary-side switching control circuit 70.

In a third inner layer L4, there are provided a pair of ground films 48, 58; a wiring area 88 for the primary side circuits 32, 34; and a wiring area 90 for the secondary-side switching control circuit 70.

Accordingly, as shown in FIG. 4, in the transformer T, the primary winding 30, the first secondary winding 40, the second secondary winding 50, the ground layer L4, and the primary winding 30 are provided in that order. Namely, two secondary windings 40, 50 are disposed on different layers L2, L3. Further, the secondary winding 40 and the secondary winding 50 are drawn out in the opposite directions each other, as shown in FIG. 3.

Together with the layouts illustrated above, the primary side circuits 32, 34, and the secondary side circuits 42, 44, 52, 54, L1 and L2 are disposed. Further, the output pattern film 56 of the second secondary winding 50 is disposed on the first inner layer L2, on which the

first secondary winding 40 is disposed. Also, the output pattern film 46 of the first secondary winding 40 is disposed on the second inner layer L3, on which the second secondary winding 50 is disposed. Corresponding to these layouts, the ground films 48, 58 are provided on the third inner layer L4.

Namely, two secondary windings 40, 50 are drawn out in the opposite directions each other. In order to connect, through via among the layers, points p1, u1, q1, s1, t1, p2, u2, q2, s2, and t2 on the secondary side circuit shown in FIG. 1, the rectifier circuits 42, 44 provided on the secondary side circuit are disposed on one side of the transformer T, while rectifier circuits 52, 54 provided on the secondary side circuit are disposed on the other side of the transformer T. Further, smoothing circuits L1, L2, and C are disposed separately on both sides of the transformer T.

According to the present invention, two secondary windings 40, 50 are disposed on the different layers L2, L3, respectively, so that large exclusive areas of secondary windings 40, 50 can be prepared in the vertical direction in the figure. In other words, a secondary winding pattern having a large cross section area S and a short pattern length l can be provided, as shown in FIG. 3.

As described earlier, a pattern resistance value is represented by $r = \rho * l / S$. Therefore, with the above-mentioned structure, the resistance value of the

pattern can be reduced. Further, because an inductance L of the pattern is proportional to the pattern length l, the inductance can be reduced.

With such a configuration, no layer dedicatedly to the output pattern films can be provided. According to the present invention, this problem is solved by arranging the extraction of the secondary windings 40, 50 in the opposite directions each other. Namely, the output pattern film 56 of the second secondary winding 50 is provided on the first inner layer L2 having the first secondary winding 40. Also, the output pattern film 46 of the first secondary winding 40 is provided on the second inner layer L3 having the second secondary winding 50.

Because these output pattern films are provided on the different layers, it becomes possible to have a large pattern width (cross section S). This enables reduced resistance values of the output pattern films, which are derived from the formula of the pattern resistance value $r = \rho * l / S$.

Similarly, the ground films 48, 58 can be disposed respectively on the right area and the left area of the third inner layer L4, thereby producing a large pattern width (cross section S). Thus, the pattern resistance value can be reduced, which is also derived from the pattern resistance value $r = \rho * l / S$.

For example, as compared to the conventional configuration shown in FIG. 9, the pattern width becomes

larger in each layer, and each pattern resistance r_a , r_c and r_g becomes half as large as in the case of the conventional configuration. Accordingly, the power loss can be reduced half as much as in the conventional method.

5 Also, switching noise can be reduced because of the smaller inductance of secondary windings 40, 50.

As shown in FIG. 10, in the conventional art, the pair of secondary windings is drawn out in an identical direction, and moreover, is disposed on an identical layer. These
10 structures produce narrow secondary windings, formed of long patterns. Further, because of the extraction in one direction, the output pattern films and ground films have to be located on each half portion of the second and the third inner layers, which disables pattern films from being
15 widened.

In contrast, according to the present invention, as shown in FIG. 1 and FIG. 5, two secondary windings transformer-coupled with the primary winding are drawn out in both directions, and disposed on different layers.
20 Therefore, the secondary windings can be structured of wide and short patterns. Moreover, because of this extraction in both directions, it becomes possible to allocate the output pattern films and the ground films on both sides of the second and the third inner layers. Thus it becomes
25 possible to produce wide pattern films.

With such measures, even when output current becomes large, the power loss becomes half as much as in the

conventional method, and higher power efficiency can be obtained. Further, switching noise can be reduced because of the reduced inductance. Moreover, the module can be structured without increasing the size.

5 [Electronic apparatus]

FIG. 7 is a configuration diagram of a board for an electronic apparatus, on which a power supply module in accordance with the present invention is mounted. FIG. 8 is a configuration diagram of an electronic apparatus, in which the board for the electronic apparatus shown in FIG. 10 7 is accommodated.

As shown in FIG. 7, a large number of LSIs 22 including a CPU are mounted on a printed circuit board 21 of a CPU board 20. A power connector 1 is provided on this board 21, and the power supply module 10 having been explained 15 in FIG. 1 through FIG. 6 is connected to the power connector 1. In this example, a plurality of (three) power supply modules 10 are mounted, because high-speed CPUs requiring large current are used.

20 As shown in FIG. 8, a required number of CPU boards 20 are vertically disposed in parallel on a rack 25, thereby constituting a server. In such a way, the power supply module 10 may be used for a distributed power supply, because of a miniaturized structure. Further, because of the improved 25 power efficiency as described earlier, it becomes possible to reduce power consumption of the electronic apparatus having high-speed CPUs which requires a large current.

[Other embodiments]

In the aforementioned embodiments of the present invention, two secondary windings are provided, as shown in FIG. 6, and one output is produced therefrom. Instead, 5 it may also be possible to have two outputs. Similarly, it may be possible to increase the number of secondary windings, to three or more, by increasing the number of layers in the module.

As the embodiments of the present invention have been 10 described, it may be possible to conceive a variety of modifications within the scope of the present invention. The foregoing description of the embodiments is not intended to limit the invention to the particular details of the examples illustrated. All features and advantages 15 of the invention which fall within the scope of the invention are covered by the appended claims.

As described above, according to the present invention, a pair of secondary windings transformer-coupled with the primary winding are drawn out in both directions, and 20 disposed on different layers. Therefore, the secondary windings can be structured of wide and short patterns. Moreover, because of this extraction in both directions, it becomes possible to allocate the output pattern films and the ground films on both sides of the second and the 25 third inner layers. Thus it becomes possible to produce wide pattern films.

With such measures, even when output current becomes

large, the power loss becomes half as much as in the conventional method, and higher power efficiency can be obtained. Further, switching noise can be reduced because of the reduced inductance. Moreover, the module can be
5 structured without increasing the size.